

2 **Methods to eliminate stimulus transduction artifact from insert earphones during**  
3 **electroencephalography**

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## Précis

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This technical note documents three approaches to the problem of stimulus transduction artifact during EEG measurement. We use insert earphones (Etymotic ER-4B) for reproduction of high frequency, high-fidelity acoustical information, and a non-specialized digital EEG acquisition system. Such standard EEG equipment has considerable potential for revealing how multiple levels of auditory processing reflect peripheral damage and lead to behavioral impairments. In this setting, the stimulus transduction artifact can contaminate scalp-recorded electrical responses to click stimuli thus compromising the fidelity of clinically relevant auditory brainstem responses (ABRs). Further, with longer complex stimuli such as speech, this artifact can temporally overlap long epochs of the EEG responses, thus confounding their interpretation. Three methods are shown to eliminate the artifact (counter-phasing, referencing, and shielding).

(121 words)

## Abstract

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Objective: To reduce stimulus transduction artifacts in EEG while using insert earphones.

Design: Reference Equivalent Threshold SPLs (RETSPLs) were assessed for Etymotic ER-4B earphones in fifteen volunteers. Auditory brainstem responses (ABRs) and middle latency responses (MLRs) – as well as long-duration complex ABRs – to click and /da/ speech stimuli were recorded in a single-case design.

Results: Transduction artifacts occurred in raw EEG responses, but they were eliminated by shielding, counter-phasing (averaging across stimuli 180° out of phase) or re-referencing.

Conclusions: Clinical-grade ABRs, MLRs, and cABRs can be recorded with a standard digital EEG system and high-fidelity insert earphones, provided one or more techniques are used to remove the stimulus transduction artifact.

(111 words)

Key words: ABR, cABR, ER-4B, headphones, RETSPL

## 1 Introduction

2 This research focuses on the measurement of neural events in the first tens of milliseconds after  
3 the onset of a sound. ABRs are used routinely for this purpose in the field of audiology. Clinical  
4 systems typically present thousands of short sounds such as 0.1-msec clicks, then average one  
5 electrode's EEG signal within a short time-epoch segment (e.g., from -2 to 10-msec post-  
6 stimulus onset). However, the acoustical world is largely comprised of complex, long-duration  
7 sounds including both speech and music. As with traditional click-ABRs, complex ABRs  
8 (cABRs) to such sounds encode onsets, but cABRs also reflect key properties of the ongoing  
9 acoustical waveform, including envelope and fundamental frequency information (for a review,  
10 see Skoe and Kraus 2010). As such, cABR investigations have the potential to improve our  
11 understanding of hearing impairment.

12 Within clinical systems, it is common to permit brief epochs of only ten to twenty  
13 milliseconds. This precludes measurement of cABRs to complex sounds, as well as middle  
14 latency responses (MLRs), and Long Latency Responses (LLRs) such as the auditory N1 or  
15 mismatch negativity (Hall, 2006:pg.2, Campbell & Neuvonen 2007, Campbell, Winkler, &  
16 Kujala 2005, 2007, Campbell, Winker, Kujala et al. 2003, for a review, see Näätänen and  
17 Winkler, 1999). Note that a few extant clinical systems do permit recordings of longer epochs,  
18 though this is not a basic feature but rather requires an add-on. Furthermore, even those systems  
19 have relatively small numbers (<10) of electrodes. For instance, Intelligent Hearing Systems  
20 SmartEP appears to lead the field with an 8-channel recording system, with an optional  
21 P300/MMN module. The Natus Bio-logic auditory evoked potential system offers a similar add-  
22 on with a 2-channel recording system. This precludes the use of techniques to localize the  
23 cortical generators of auditory Long Latency Responses and therefore, as discussed below, relate  
24 peripheral activity (ABRs) to its central neural and perceptual consequences. Thus users of

1 clinical auditory evoked potential systems, even with add-ons, often do not have these tools  
2 available to them.

3         Conversely, users of ordinary digital EEG systems (Fisch & Spehlmann, 1999; Swartz,  
4 1998), which measure longer responses and signals from multiple electrodes, are largely unaware  
5 that their system might also be used to acquire ABRs. That is, there are investigators with  
6 clinical systems who cannot measure later responses, and those with ordinary digital EEG  
7 systems who do not appreciate that they may be equipped to acquire ABRs as well. The ability  
8 to measure both ascending brainstem and later cortical responses, and to characterize their  
9 relationships, would have not only clinical but also basic scientific import.

10         Peripheral sensorineural damage is the most common origin of hearing impairment  
11 (Yueh, Shapiro, MacLean et al, 2003). As this damage limits the information available to the  
12 brain, the auditory periphery remains the focus of most clinical efforts. However, a more  
13 integrated view of the auditory system is necessary to understand the varied central  
14 consequences of peripheral loss (Shinn-Cunningham & Best, 2008; Pichora-Fuller & Singh,  
15 2006) and to characterize the multiple forms of hearing impairments that are not of peripheral  
16 origin, which fall under the umbrella term of Central Auditory Processing (CAP) abnormalities  
17 (Banai & Kraus 2006; 2008). CAP is a major public health problem, shown to have a prevalence  
18 of 76.4% in a population of individuals over the age of 55 years (Golding et al. 2004).  
19 Furthermore, central adaptation to peripheral impairment over the course of our lives without an  
20 aid can also affect whether rehabilitation is necessary or possible after an aid is fitted (Woods &  
21 Yund 2007).

22         Understanding the peripheral and central mechanisms of hearing, as well as their relation,  
23 will be fundamental in advancing both the basic science of hearing and clinical practice, as it

1 could lead to biomarkers that offer specificity for treatment. In this regard, clinical systems that  
2 are specialized for ABR measurement do not allow measurement of longer thalamocortically-  
3 generated MLRs. A basic purpose of the present work is thus to demonstrate if ABRs to click  
4 and speech stimuli, together with MLRs, and the long-lasting cABR responses to speech stimuli  
5 (Skoe & Kraus, 2010) can be recorded simultaneously via one ordinary digital EEG system. This  
6 feature of simultaneous recording is not a capability of the current state-of-the-art in clinical  
7 auditory evoked potential systems. A second purpose is to identify technical recommendations  
8 for presentation of complex auditory stimuli during such a measurement, to which we now turn.

9       Stimulus transduction artifacts occur when stimulus-producing current in the headphone  
10 wire or transducer, proximal to the body or electrode components, contaminates the EEG  
11 measurement. The acoustical waveform mirrors aspects of the stimulus-producing current.  
12 Clinical systems use several common ways of avoiding the artifact. One is to present very brief  
13 stimuli (clicks) so the artifact ends before the ABR is evident (<1-msec). However, this does not  
14 work for realistic stimuli, which overlap in time with their cABRs (Skoe & Kraus, 2010).  
15 Another method is to deliver stimuli pneumatically via plastic tubes, where the transducer is  
16 situated at a distance of up to 20 feet from the patient (Killion 1984); e.g., the Etymotic ER-3A  
17 (Henry et al. 2001, Hall 2006:pg.71). Stimulus transduction artifact has been shown to be  
18 eliminated by grounded shielding of the electrical apparatus from such a system (Akhoun,  
19 Moulin, Jeanvoine, et al. 2008; Riazi & Ferraro 2008), even when that apparatus was close to the  
20 volunteer. However, such earphones are costly and have an inferior frequency response for  
21 sounds above 6-7 kHz (Henry et al. 2001), an important range for spatial localization and speech  
22 cues (consonant stops). For instance, high frequency cues contribute to the perception of sibilants  
23 and fricative sounds by children during middle childhood (Stelmachowicz et al., 2001; 2008). An

1 additional shortfall of tubing is that of acoustic dispersion, whereby the low frequency  
2 components of sounds travel faster than high frequency components within a tube, such that the  
3 phase relations of different frequency components becomes distorted: e.g., a click can become  
4 smeared into a frequency-modulated sweep or “chirp” (Kinsler et al. 1982). The frequency  
5 response and fidelity of the pneumatic approach thus has limitations for those interested in the  
6 responses to everyday complex stimuli such as speech or music sounds, but the problem is also  
7 relevant for click stimuli (Kinsler et al. 1982). The tubing approach does offer a solution to the  
8 problem of stimulus transduction artifact should: i) the investigation not require high fidelity  
9 reproduction of sound and, ii) should the investigation not need the reproduction of high  
10 frequency information such as speech or location cues.

11         Typical lower cost solutions to the stimulus transduction artifact include “counter-  
12 phasing”, where EEG responses to two versions of the same stimulus with opposing polarity  
13 cancel out the artifact (Hall 2006: pg.248, Aiken & Picton 2008, Skoe & Kraus 2010), and  
14 referencing, where the EEG signal is compared to an equally contaminated electrode so the  
15 artifact is Common-Mode Rejected (Fisch & Spehlmann, 1999). A third approach that we  
16 explore here is electrically-shielding the headphone wire with a grounded Faraday cage of  
17 conducting mesh.

18         With a view to the high-fidelity reproduction of speech cues as is ideal for cABRs to  
19 speech sounds, here we used the Etymotic ER-4B earphones (Henry et al. 2001). ER-4Bs are of  
20 a very different construction from the ER-3As that are the current state-of-the-art in clinical  
21 evaluations. The ER-4B could in theory induce greater artifact, having wires right up to the ear  
22 and the transducer in the ear canal. To determine whether auditory responses to click and /da/  
23 speech stimuli during the first 60-msec can be measured with an ordinary digital EEG system

1 (Fisch & Spehlmann, 1999; Swartz, 1998) and personal computer, here we test the effectiveness  
2 of three low cost approaches – counter-phasing, referencing and shielding – to the eliminate  
3 stimulus transduction artifact from ER4-B earphones.

#### 4 Materials and Methods

5 Participants. 15 individuals (6 males) aged 18 years 10 months to 28 years 11 months old (mean  
6 age: 22 years 6 months, standard deviation, 2 years 9 months) participated in the audiogram  
7 calibration sessions, having reporting normal hearing (Cox & Alexander 1995) without a history  
8 of i) ear infections or injury, ii) regular firearms use, or iii) working in clubs, construction, or  
9 other loud situations. A 23-year old male with self-reported normal hearing participated in the  
10 EEG measurements reported here. In accordance with the Declaration of Helsinki, all  
11 participants gave informed written consent with ethical approval by the campus Institutional  
12 Review Board.

13 RETSPL Measurement. RETSPLs for Etymotic (Elk Grove Village, Illinois, USA) ER-4B  
14 earphones (Henry et al. 2001) with ER4-18 3-flange eartips were determined with an automated  
15 audiogram procedure. dB SPL values were measured using a Brüel & Kjær 4157 ear-simulator  
16 attached to a Larson Davis ½” preamplifier. dB SPL values were calibrated to a 1000 Hz tone  
17 from a Larson Davis Cal200 acoustic calibrator. Participants were instructed to press a computer  
18 key in response to hearing a tone. Pure tones (125 to 16000-Hz; Table 1) were presented for 200-  
19 msec with a 20-msec linear onset and offset ramp with 1000 to 1500-msec jittered delay. Each  
20 frequency × ear (13 × 2) was tested in random order using an automated version of the modified  
21 Hughson-Westlake ANSI S3.21-1978 (R-1992) procedure, starting at a below threshold volume,  
22 with a 10 dB increase on misses and a 5 dB decrease for hits, requiring a 2/3 ascending hit/miss  
23 ratio to determine each threshold. Using the RETSPL values derived from the average of the



1 calibration participants, the EEG participant's audiometric thresholds were determined to be  
2 better than 20 dB HL at all frequencies, as tested before and after the EEG session.

3 EEG recording session. A single participant was situated in a chair within an acoustically- and  
4 electrically-shielded chamber where he watched a silent subtitled movie of his choice, while  
5 EEG was measured and sound presented via the right earphone. The level of the sound was  
6 determined to be 80 dB(C) beforehand by the comparison of an acoustical recording of the  
7 stimulus to that of a 1kHz pure tone reference produced by a Larson Davis Cal200 acoustic  
8 calibrator. These recordings were made via a Brüel & Kjær 4157 ear-simulator attached to a  
9 Larson Davis ½" preamplifier. This comparison used the root mean square of the reference  
10 recording and the peak of the stimulus recording, filtered with a C frequency-weighting as  
11 implemented in MATLAB 7.4.0(2007a); a form of filtering that approximates the sensitivity of  
12 the human auditory system at the moderate sound levels used in this study (Moore 2003: pg.  
13 130). Neurobehavioral Systems Presentation software (Albany, California, USA) is a crucial  
14 element of the paradigm, as it controlled event timing to within 0.1msec. ER-4B wires were  
15 either unshielded or shielded, depending on the experimental condition. Shielding was comprised  
16 of tinned-copper mesh (Scotch 24 electrical shielding tape, Austin, Texas, USA) wrapped around  
17 the length of the wire, attached to the electrical ground, and insulated with low-voltage  
18 Plymouth/Plymouth-Yonshue (Canton, China) vinyl electrical tape with rubber-based adhesive .

19 The experimental session began with 16 blocks of EEG recording. Blocks lasting 3  
20 minutes 3 s contained 4 trains of 1056 1-msec clicks with linear rise and abrupt offset at  
21 Stimulus Onset Asynchrony (SOA) 40-msec, while blocks lasting 6 minutes 12 s contained 8  
22 trains of 480 40-msec /da/ stimuli (SOA: 90-msec). A 1-ms duration click was used to ensure  
23 any transduction artifact, if present, would be identified in the EEG signal, collected at a sample

1 rate of 16384 Hz. Speech stimuli were synthesized by Praat (Boersma & Weenink 2010). The  
2 SOA between the last click of train and the first click of the next train was 4.800 s and the SOA  
3 between the last /da/ of a train and the first click of the next train was 3.890 s. Leading phase  
4 (condensation, rarefaction) was randomized within blocks presented in counterbalanced order.  
5 Electrophysiological Recording Equipment. Digital EEG and Electroculogram (EOG) was  
6 acquired via a Biosemi ActiveTwo system (Amsterdam, The Netherlands). Each scalp electrode  
7 within this system is described as “active” by virtue of containing a pre-amplifier that  
8 dramatically reduces impedance before the signal travels along the wires to the amplifier and  
9 analog-to-digital converter. These electrodes used here are described as ‘standard’, in contrast to  
10 the ultra-flat active electrode components of the Biosemi ABR option, which could provide an  
11 even lower internal input noise and higher gain in the amplification selectively within the 100-  
12 3000 Hz pass band. Within this pass band resides the EEG power of the ABR, but not that of  
13 MLR and LLR signals. Our measurements are thus a test of sufficiency for these standard  
14 electrodes – which can be used to measure MLRs and LLRs– to also measure ABRs and cABRs.

15 The Biosemi ActiveTwo replaces the classical “ground” electrode with two electrodes.  
16 These are the Common Mode Sense active electrode that detects the effects upon the participant  
17 of current return from the Analog-to-Digital convertor via the Driven Right Leg (DRL) electrode  
18 that contains no amplifier. A CMS/DRL feedback loop equates the potential of the participant to  
19 the reference voltage of the Analog-to-Digital Conversion box. EEG was acquired at a scalp  
20 electrode in “raw” mode, that is, relative to this reference voltage. Thus the “reference” in “raw”  
21 recordings was the CMS electrode, which was situated at a right-posterior site between POz and  
22 PO4. This “raw” mode of recording did not permit the full Common Mode Rejection (Fisch &  
23 Spehlmann, 1999) of extraneous signals, such as stimulus transduction artifact that was present

1 at both an EEG electrode and the CMS. These “raw” measurements are thus a test of the  
2 effectiveness of methods of counter-phasing and shielding without Common Mode Rejection by  
3 re-referencing.

4 EEG and EOG acquisition parameters. EEG was acquired in “raw” mode at CPz relative to a  
5 CMS reference with a pass band of DC to 3334Hz and sampled at 16384 Hz. Horizontal eye  
6 movements were monitored with a bipolar set-up, with two electrodes attached laterally to the  
7 outer canthi of each eye. Vertical eye movements were monitored by bipolar channels using pre-  
8 frontal electrodes (Fp1, Fp2) amplified against an electrode upon the tip of the nose. Electrodes  
9 were also attached to the mastoids.

10 Derivation of ABR, cABR, and MLR responses. For ABRs/cABRs, EEG/EOG was filtered  
11 offline (70- to 2000-Hz) and subsequently analyzed with EEGLAB (Delorme and Makeig,  
12 2004)\*. The “raw” EEG/EOG data was retained, but also re-referenced offline to the right  
13 mastoid to permit Common Mode Rejection (Fisch & Spehlmann, 1999) of stimulus transduction  
14 artifact. Analyzing raw and re-referenced data separately, EEG/EOG data were epoched,  
15 baseline-corrected, artifact-rejected and averaged; mathematical processes that are detailed  
16 below. Continuous time-series of EOG/EEG data were segmented or “epoched” into shorter time  
17 series of electrophysiological data. The “epochs” began 6-ms before the onset of each sound and  
18 ended 60 ms after the onset of each sound. The electrophysiological data in the first 6 ms of each  
19 66-ms epoch was used to determine a mean pre-stimulus baseline value for each  
20 electrophysiological channel (e.g., CPz), which was then subtracted from every data point in that  
21 channel for the whole epoch; a process that is termed “baseline correction”. Epochs were then  
22 “artifact-rejected”, that is, these epochs were excluded from the subsequent averaging process if  
23 that baseline-corrected epoch contained potentials  $\pm 50\text{-}\mu\text{V}$  within any EEG or EOG channel.

1 Also, the first and last two sounds of a block, together with events immediately before, during or  
 2 immediately after timing jitter greater than 1 sample (61.03- $\mu$ sec) were excluded from the  
 3 subsequent averaging process. Means of the electrophysiological data at each corresponding  
 4 time point, in each corresponding channel, for each of the remaining epochs was taken to derive  
 5 the averaged responses of interest. That is, for each combination of stimulus (click, /da/),  
 6 reference (raw, re-referenced) and shielding (shielding, unshielded), responses time-locked to  
 7 stimuli were averaged from accepted epochs containing sounds of i) condensation and ii)  
 8 rarefaction leading phase, as well as iii) collapsed across leading phase. To reveal MLRs,  
 9 EEG/EOG was filtered (15 to 2000-Hz), re-referenced and responses similarly derived. These  
 10 averaged responses derived from the CPz EEG channel were then over-plotted (Figures 1-2).

## 11 Results

12 RETSPL values for the Etymotic ER-4B insert phones are depicted in Table 1.

13 -----  
 14 [PLEASE INSERT TABLE 1 ABOUT HERE]  
 15 -----

16 As illustrated below, comparison of the stimulus waveform (Figures 1a-d) to this individual's  
 17 'raw' ABRs to stimuli revealed that a stimulus transduction artifact was superimposed upon the  
 18 ABR; an artifact that corresponded to whether the sound had a condensation or rarefaction  
 19 leading phase. This correspondence was seen when headphone wires were unshielded (Figures  
 20 1e and 1g) during the interval that the sound was presented. This artifact was no longer  
 21 superimposed upon the analogous ABRs following counter-phasing (Figures 1e & 1g;  
 22 "collapsed" in black), or referencing (Figures 1i and 1k). Shielding (Figures 1b, 1f, 1j, 1d, 1h, 1l)

1 also removed this superimposed artifact. Referencing revealed the ABR deflections denoted  
 2 upon Figure 1i-1l.

3 -----  
 4 [PLEASE INSERT FIGURE 1 ABOUT HERE]  
 5 -----

6 The responses depicted over a longer time range in Figure 2e-p again revealed that  
 7 artifacts superimposed onto these longer responses, in a manner that was confined to raw  
 8 waveforms without counter-phasing and shielding. The artifact for /da/ (Figure 2g) resembled  
 9 the longer stimulus waveform (Figures 2c-d). Whether counter-phased or not, shielded or not, re-  
 10 referenced waveforms (Figure 2i-l) revealed deflections of the cABR (Figure 2k and l) that did  
 11 not reflect the timing and polarity of the transduction artifact, but rather corresponded to  
 12 landmarks (Figures 2c-d) within the stimulus waveform; albeit time-shifted by a ca. 8-msec  
 13 delay (Skoe and Kraus, 2010). These cABR deflections were not seen in the click ABRs, which  
 14 instead contained an ABR to the subsequent click (Figure 2i-j). MLRs were seen with an open  
 15 filter (Figure 2m-p) for clicks and /da/ stimuli (black labels) onto which were superimposed the  
 16 ABR and cABR deflections (grey labels).

17 -----  
 18 [PLEASE INSERT FIGURE 2 ABOUT HERE]  
 19 -----

## 20 Discussion

21 The results showed that a transduction artifact occurred only when both the headphone  
 22 wire was not shielded, and the data was not re-referenced. In this case, counter-phasing still  
 23 proved effective in eliminating transduction artifact. Accordingly, counter-phasing, shielding,

1 and referencing were all effective in removing the transduction artifact from ABRs and cABRs.  
2 Re-referenced data revealed ABRs (Figure 1) and MLRs (Figure 2) to click and /da/, and a  
3 cABR to /da/ (Figure 2). Without these methods for removing transduction artifact, e.g., without  
4 grounded-shielding, 'raw' uncollapsed ABRs (Figures 1e and 1g) to stimulus onset and cABRs  
5 (Figure 2e and 2g) to aspects of the ongoing speech waveform were contaminated by super-  
6 imposed stimulus-producing currents. The problem is more serious when the cABR responses of  
7 interest are to landmarks in that ongoing stimulus waveform (Skoe and Kraus, 2010), such that  
8 artifact could be mistaken for a cABR response. That these cABRs were elicited in the same time  
9 range as MLRs yet followed a different additive time course indicated that cABRs are not MLRs.  
10 In this investigation, one ordinary digital EEG system was thus used to simultaneously measure  
11 artifact-free ABRs, MLRs and cABRs to long-lasting speech sounds. The novel aspect of this  
12 investigation is that the established techniques of counter-phasing, shielding, and referencing  
13 proved effective when stimuli were presented via a device capable of the high-fidelity  
14 reproduction of speech cues for ABR and cABR investigations: the ER4-B. This allows us to  
15 make technical recommendations for artifact-free recordings upon presentation of complex  
16 auditory stimuli via such earphones for similar investigations. Below we consider the generality  
17 and nature of each approach to artifact elimination.

18         The applicability of counter-phasing depends upon the research question and subsequent  
19 analyses. That is, counter-phasing offers no solution to the problem of transduction artifact for  
20 those interested in the effects of leading phase upon early waves of the ABR (Schoonhoven  
21 1992), for instance with inter-trial phase coherence (Delorme and Makeig 2004), which may bear  
22 perceptually-relevant information.

1           The effectiveness of referencing depends upon numerical equivalence of the amplitude of  
2 artifact at data and reference electrodes. Such equivalence is likely when the transduction artifact  
3 reflects mainly a current induced within the human body that reaches the sensors by volume  
4 conduction, as could be the case in the reported data. Were transduction artifact due to  
5 electromagnetic interference from the earphone wire's field, within which the scalp and  
6 reference electrode wires are situated, the spatial proximity or orientation of each electrode wire  
7 to the earphone wire would be critical to the effectiveness of referencing. The best choices of  
8 reference electrode(s) depends upon the research question (Fisch & Spehlmann 1999), so if such  
9 electromagnetic interference were a key source of transduction artifact (Hall 2006), it could  
10 prove impossible to maximize the EEG signal of interest while eliminating the artifact via  
11 referencing alone.

12           Grounded shielding proved effective here, and this is probably due to the containment of  
13 the electromagnetic field produced by earphone wire currents. Without shielding, this field is  
14 thought to have induced a stimulus transduction artifact in the volunteer's body that reached the  
15 electrodes via volume conduction. The transducer itself remained unshielded throughout, yet the  
16 transduction artifact was basically eliminated by shielding the wires alone. The primary origin of  
17 stimulus transduction artifact is thus the current in the earphone wire, rather than the balanced-  
18 armature transducer of the ER-4B. As noted in the Introduction, grounded shielding of the  
19 electrical apparatus has proved successful in eliminating transduction artifact with systems that  
20 deliver stimuli via pneumatic tubes (Akhoun et al. 2008; Riazi & Ferraro 2008). Grounded  
21 shielding approaches could have considerable potential in the investigation of the cochlear  
22 microphonic and ABRs in early life, as they could improve approaches to the early diagnosis of  
23 auditory neuropathy (Riazi & Ferraro 2008). However, earphones that deliver stimuli via

1 pneumatic tubes suffer from acoustic dispersion (Kinsler et al. 1983) and offer an inferior  
2 representation of high frequencies (Henry et al. 2001); information that is important for speech  
3 recognition and spatial localization. A distinct approach, shielding the wiring yet not the  
4 transducer, was shown here to eliminate transduction artifact from lower cost ER4-B headphones  
5 that are viable for presentation of speech content for ABR and cABR investigations, and the  
6 presentation of high frequency auditory localization cues. While the ER3-A is the current state-  
7 of-the-art in routine clinical use, the ER4-B would show further clinical promise, should aspects  
8 of the neural processing of speech stimuli or auditory localization cues, as reflected by ABRs,  
9 cABRs or MLRs, become established as biomarkers that offer specificity for treatment. In the  
10 absence of such biomarkers that index aspects of the auditory system's response to stimuli  
11 presented via the ER4-B, the additional clinical utility of the ER4-B is still necessarily an  
12 empirical question.

13         Other empirical challenges also remain. One limitation of simultaneously recording  
14 responses from several levels of the auditory system is the difficu

15         lty in finding a single stimulus and set of stimulus parameters that are optimal for all the  
16 responses. For instance, different evoked potential components exhibit, in a different manner, the  
17 property of "refractoriness", where components become progressively attenuated upon repeated  
18 stimulation, recovering after a period of silence (Alciani et al, 1995; Campbell et al. 2003). In  
19 cortex, the optimal SOA for recording the N1 component is 1.5 seconds (Campbell et al. 2005).  
20 By contrast, the refractory period of wave V of the ABRs to a repeated click is 30 ms (Picton et  
21 al. 1981) and the optimal SOA somewhat shorter. Thus when simultaneously recording  
22 components from several levels, some degree of compromise is inevitable. However, we show  
23 here that ABRs and cABRs may be recorded alongside MLRs. Indeed, it is also possible to



1 measure LLRs simultaneously with ABRs and MLRs (Woldorff et al. 1987; Woldoff et al.  
2 1991), provided SOAs are jittered to allow techniques such as Adjard correction when necessary  
3 (Woldorff, 1993). Whether ABRs, cABRs, MLRs and LLRs can be simultaneously recorded  
4 will therefore depend on the experimental constraints. When they can, the potentially clinically-  
5 relevant interaction of responses at different levels of the auditory system can then be assessed.

6 A further challenge is that studies of the electrical auditory brainstem response (EABR)  
7 and the electrical auditory middle latency response (EAMLRL) to electrical stimulation via  
8 various implanted arrays of electrodes (Starr & Brackmann, 1979; Waring et al. 1998; Firszt et  
9 al. 2002) are often fraught with technical difficulties due to stimulus transduction artifact. The  
10 applicability of variants of the techniques outlined here to the electrically-evoked responses of  
11 cochlear and brainstem implants remains both a technical challenge and an empirical question.

12  
13 Conclusions. ABRs to click and speech stimuli, MLRs, and long-lasting cABR responses can be  
14 recorded simultaneously via one ordinary digital EEG system. Such equipment thus has promise  
15 for investigations that intend a more integrated approach to the auditory system in improving our  
16 understanding of hearing and hearing disorders, particularly when long-lasting responses such as  
17 MLRs and cABRs to long-duration artifact-producing stimuli are of interest. Counter-phasing,  
18 referencing and shielding each eliminated stimulus transduction artifact that originated primarily  
19 from stimulus-related current in the earphone wire. A combination of all three techniques is  
20 recommended, where appropriate, to permit the measurement of auditory responses including  
21 ABR/cABR and MLR with ordinary digital EEG hardware using ER-4B earphones.

22

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## 1 Table and Figure Legends

2 Table 1. RETSPL as a function of tone frequency for Etymotic ER-4B insert phones with ER4-  
3 18 3-flange eartips, referenced with a Brüel & Kjær 4157 ear-simulator (N= 15).

4 Figure 1. The stimulus waveform (a-d) used to elicit ABRs (e-l) that are plotted as a function of  
5 shielding, reference and leading phase. Please note the different scale for the referenced  
6 waveform where ABRs are visible and the large artifact eliminated. ABR peaks are labeled by  
7 Jewett-nomenclature.

8 Figure 2. The stimulus waveform (a-d) used to elicited cABRs (e-l) that are plotted as a function  
9 of shielding, reference and leading phase, together with the effect of a more open filter for  
10 referenced data that yields overlapping MLRs (m-p). ABR and MLRs labels follow Jewett- and  
11 Picton-conventions; cABRs are labeled according to Skoe and Kraus (2010), as are  
12 corresponding landmarks in the stimulus waveform.

13

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1

## Footnote

2

\*ERPs can be derived using the ERPLAB plugin (<http://erpinfo.org/erplab/>) to EEGLAB.

3

4



1 Table 1.

Frequency	RETSPL
125	54.08
250	38.25
500	24.04
750	18.85
1000	16.42
1500	18.88
2000	22.03
3000	21.37
4000	19.39
6000	18.43
8000	17.26
11200	27.20
16000	51.83

2

Figure 1

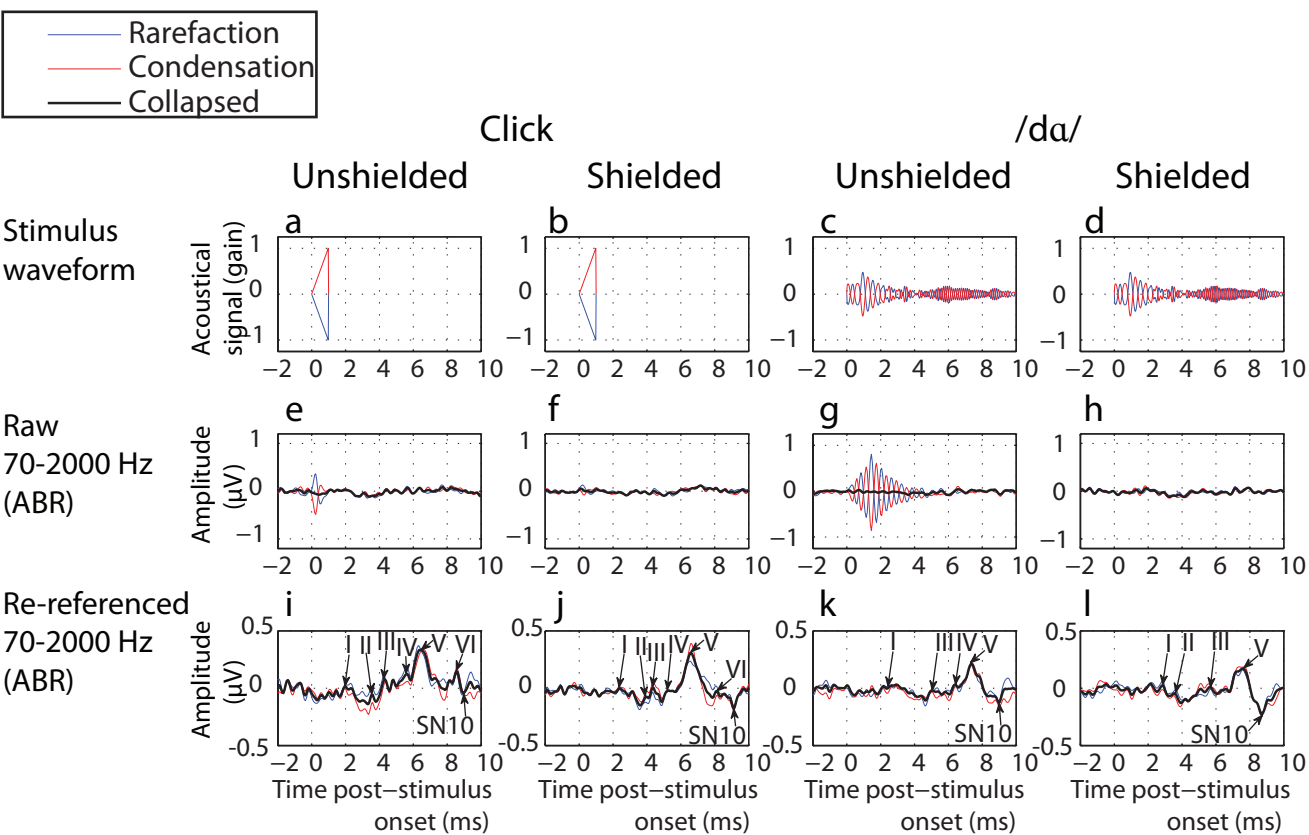


Figure 2

